1574

50464

Index on page 3.

1575

		L1	C	B1		
789		-11.9 / 538	-1.1 / 10.0	-0.6	-0.4 / 10.0	-6.2 / 30.6
788		-5.2 / 30.4	-0.0 / 10.0	-2.4	-3.7 / 10.0	-4.0 / 13.7
787		-1.1 / 12.2	-0.4 / 10.0	-2.0	-0.9 / 10.0	-5.0 / 30.0
786		-0.9 / 11.3	-1.1 / 10.0	-1.9	-2.9 / 10.0	-4.8 / 19.6
785		-1.0 / 10.7	-0.4 / 10.0	+0.7	-1.5 / 10.0	-8.5 / 27.0
784		-1.6 / 13.4	-1.9 / 10.0	-1.5	-1.0 / 10.0	-12.0 / 34.0
783		-8.0 / 14.1	-0.5 / 10.0	-0.2	-0.6 / 10.0	-13.7 / 37.4
782		-0.6 / 21.2	-1.8 / 10.0	-0.6	-0.4 / 10.0	-0.8 / 10.8
781		-0.9 / 11.8	-0.7 / 10.0	+0.1	-0.1 / 10.1	-0.7 / 11.4
780			+0.4 / 10.0	+0.8	-0.5 / 10.0	-1.3 / 12.2
779			-0.0 / 10.0	+1.3	+0.7 / 10.0	
824		-7.0 / 24.6	-6.7 / 10.0	-4.4	-6.5 / 10.0	-14.3 / 32.6
825		-8.2 / 26.4	-7.1 / 10.0	-6.8	-8.4 / 10.0	-16.7 / 38.2
826		-6.2 / 22.7	-4.7 / 10.0	-4.7	-6.1 / 10.0	-14.9 / 33.8
827		-13.6 / 37.0	-8.7 / 10.0	-7.9	-8.4 / 10.0	-19.1 / 43.2
828		-10.0 / 24.0	-9.7 / 10.0	-8.7	-10.7 / 10.0	-17.0 / 34.0

Nov 12, 1910.

1576

829					
830	-16.9 / 49.8	-10.1 / 10.0	-10.7	-10.4 / 10.0	-18.3 / 46.0
832	-15.6 / 47.2	-9.8 / 10.0	-11.0	-11.8 / 10.2	-15.5 / 47.2
833	-15.9 / 47.8	-18.6 / 10.0	-10.1	-10.3 / 10.2	-17.6 / 45.2
834	-17.0 / 47.8	-10.1 / 10.0	-9.5	-9.9 / 10.0	-17.5 / 45.0
835	-17.3 / 47.6	-13.6 / 10.0	-12.5	-13.1 / 10.0	-17.1 / 47.9
836	-16.8 / 43.6	-13.6 / 10.0	-12.1	-13.8 / 10.0	-19.6 / 49.2
837	-18.8 / 49.6	-19.5 / 10.0	-15.5	-14.5 / 10.0	-20.0 / 50.0
838	-16.7 / 43.2	-17.3 / 10.0	-15.1	-14.5 / 10.0	-20.1 / 50.2
839					
840					

1577

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" " at "H" 706+19.05 " "	p. 63-64
" " " "D" 743+0.5 East Approach Co. Road Bridge	p. 65
" " " "D" 777+45, Road Crossing	p. 66
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1578

Level

Elev. Grade

737 78

750 77

734 68 172

Level

Embankment Original Cross Sections continued from Original Cross Section Book No 5, page 34.

1579

D

Station	Elev	Grade	Left	℄	Right
					7
750	7.3		$-16\frac{5}{42}$ $-16\frac{7}{9}$	$-16\frac{7}{9}$	$-16\frac{8}{9}$ $-17\frac{9}{43}$
741	7.5		$-16\frac{6}{42}$ $-16\frac{5}{9}$	$-16\frac{5}{9}$	$-16\frac{6}{9}$ $-16\frac{5}{42}$
750	7.7		$-16\frac{3}{41}$ $-16\frac{3}{9}$	$-16\frac{3}{9}$	$-16\frac{3}{9}$ $-16\frac{4}{41}$
7[illegible]	7.8		$-16\frac{2}{41}$ $-16\frac{2}{9}$	$-16\frac{2}{9}$	$-16\frac{2}{9}$ $-16\frac{2}{42}$
750	8.2		$-15\frac{8}{40}$ $-15\frac{8}{9}$	$-15\frac{8}{9}$	$-15\frac{8}{9}$ $-16\frac{2}{41}$
739	8.1		$-15\frac{9}{40}$ $-15\frac{9}{9}$	$15\frac{9}{9}$	$16\frac{1}{9}$ $-16\frac{6}{42}$
750	8.2		$-15\frac{6}{41}$ $-15\frac{8}{9}$	$-15\frac{8}{9}$	$-15\frac{8}{9}$ $-16\frac{0}{41}$
738	8.1		$-15\frac{7}{40}$ $-15\frac{9}{9}$	$-15\frac{9}{9}$	$-15\frac{9}{9}$ $-16\frac{1}{41}$
750	80	23 984	$-15\frac{1}{41}$ $-15\frac{8}{9}$	$-16\frac{0}{9}$	$-16\frac{0}{9}$ $-16\frac{0}{41}$

Continued from Original Cross Section Book No 5, page 34.

1580

Elev Grade

3.3

7.3

7.8

+50 13.3

+52 7.2 23.94

1581

Station	Elev	Grade	Left		C	Right	
750	5.6		-16.0 / 45.0	-18.0 / 9	-18.4	18.7 / 11.4	-19.9 / 50.2
744	3.9		-20.2 / 43.2	-19.7 / 9	-30.1	-20.1 / 9	-19.8 / 46.2
769	4.3		-19.7 / 46.4	-19.7 / 9	-19.7	-19.7 / 9	-19.7 / 48.4
752	12.5						
750	12.6		-11.4 / 31.2	-11.7 / 9	-11.4	-11.1 / 9	-11.7 / 31.8
739	12.6		-11.4 / 31.8	-11.4 / 9	-11.4	-11.4 / 9	-11.4 / 31.8
725	5.0						
715	4.8		-19.2 / 47.4	-19.2 / 9	-19.2	-19.2 / 9	-19.2 / 47.4
705	5.5						
743	6.2	23.984	-17.0 / 43.0	-17.8 / 9	-17.8	-18.0 / 9	-18.7 / 45.4

Flagpole on Gammon barn in range

Hub on Gammon levee

S 41° W 409

992

150

145

135

150

Hub on levee

1582

Station	Elev. Grade	Left			Right		
748	6.9	-17 1 / 132	-16 9 / 9	-17 1	-17 1 / 22	-16 8 / 55 6	
750	6.5	-17 5 / 44 0	-17 5 / 9	-17 5	-17 2 / 22	17 1 / 54 2	
749	6.3	-17 6 / 44 2	-18 0 / 9	-17 2	-17 2 / 22	-17 5 / 57 2	
750	6.1	-17 6 / 44 2	-17 7 / 9	-17 3	-18 1 / 22	-17 8 / 57 6	
746	5.8	-17 8 / 44 2	-18 0 / 9	-18 2	-18 2 / 22	-18 2 / 58 4	
750	6.0	-17 5 / 44 0	-18 0 / 9	-18 2	-18 2 / 22	-18 0 / 58 0	
745	5.9	-19 4 / 47 5	-17 9 / 9	-18 1	-18 7 / 16	-18 7 -21 4 -21 4 / 26 28 45	
						18 0 / 52 2	
785	5.5						
770	3.7						
758	4.0	23 984					

1583

Station	Flow Gage			Left			Right	
753	8.0			-15⁶ 40⁶	-16⁰ 9	-16⁰	-15⁹ 22	-16³ 54⁶
" +50	7.8			15⁷ 40⁷	-16⁷ 9	-16²	-16⁰ 22⁰	-16⁴ 54⁶
752	7.9			-15⁴ 39⁸	-15⁹ 9	-16¹	-15⁹ 22	-15⁹ 53⁸
" +50	8.3			-15⁴ 39⁵	-15⁷ 9	-15⁷	-15⁹ 22	-16² 54⁴
751	8.4			-15⁴ 39⁵	-15⁷ 9	-15⁶	-15⁸ 22	-15⁸ 53⁶
" +50	8.4			-15⁶ 40²	-15⁶ 9	-15⁶	-15⁵ 22	-15⁹ 53⁸
750	8.4			-15⁶ 40²	-15⁸ 9	-15⁶	-15⁷ 22	-16⁰ 54⁰
" +50	8.2			-16⁰ 41⁹	-15² 9	-15⁸	-16⁰ 22⁰	-16⁰ 54²
						-16¹		
749	7.9			-16⁴ 41⁵	-16¹ 9	-16¹	-16⁴ 22	-16³ 54⁴
" +50	7.3	23984		-16⁹ 42⁸	-16⁷ 9	16⁷	-16⁷ 22	-16² 54⁴

15984

Station	Elev	Grade	Left		C	Right	
750	7.9		-16 1/2 41 1/2	-16 1/2 9	16 1/2	-16 2/2 22	-16 5/5 55 0
757	7.8		-16 2/2 41 2/2	-16 2/2 9	-16 2/2	-16 2/2 22	-16 6/6 55 2/2
750	7.9		-16 2/2 41 1/2	-16 2/2 9	-16 1/2	-16 0/0 22	-16 2/2 55 1/2
756	7.8		-16 2/2 41 1/2	-16 2/2 9	-16 2/2	-16 3/3 22	-16 2/2 55 1/2
750	7.7		-16 1/2 41 2/2	-16 3/3 9	-16 2/2	-16 1/2 22	-16 6/6 55 2/2
755	7.4		-16 6/6 42 2/2	-16 5/5 9	-16 6/6	-16 7/7 22	-16 7/7 55 1/2
750	7.1		-16 7/7 42 1/2	-16 5/5 9	-16 2/2	-17 1/1 22	-16 9/9 55 2/2
754	7.3		16 6/6 42 2/2	-16 2/2 9	-16 2/2	-16 7/7 22	-16 3/3 55 1/2
750	7.6		-16 2/2 41 2/2	-16 3/3 9	-16 4/4	-16 6/6 22	-16 7/7 55 1/2
753+31.8	7.6	23984 E.C.	-16 2/2 41 1/2	-16 4/4 9	-16 4/4	-16 6/6 22	-16 6/6 55 2/2

1585

Station Top Grade

753	8.4					
762	8.5					
761	8.3					
753	8.5					
733	8.6					
720	8.0					
750	7.9					
759	8.0					
750	8.0					
758	8.1	23 94				

1586

Station	Elev	Grade	Left			Right	
+50	8.0		-16 4/12	-16 2/9	-16 0	-15 6/22	16 2/54
767	7.7		-16 3/11 6	-16 3/9	-16 3	-16 1/22	-16 4/54
+50	8.0		-16 6/12	-16 1/9	-16 0	-16 0/22	-16 2/54
766	7.7		-16 6/12	-16 4/9	-16 3	-16 2/22	-16 0/54
+50	7.4		-17 4/13 4	-16 6/9	-16 6	-16 6/22	16 4/54
765	7.4		-17 1/13 2	-16 6/9	-16 6	-16 7/22	-16 2/53 4
+50	7.5		-17 0/13 0	-16 7/9	16 5	-16 4/22	-16 5/55
764	7.7		-16 7/12 4	-16 3/9	-16 3	-15 9/22	-15 9/53 6
+50	8.0		-16 3/11 6	-15 9/9	-16 0	-15 5/22	-15 1/53 4
763	8.3	23 984	-15 7/10 4	-15 9/9	-15 7	-15 8/22	-15 7/53 4

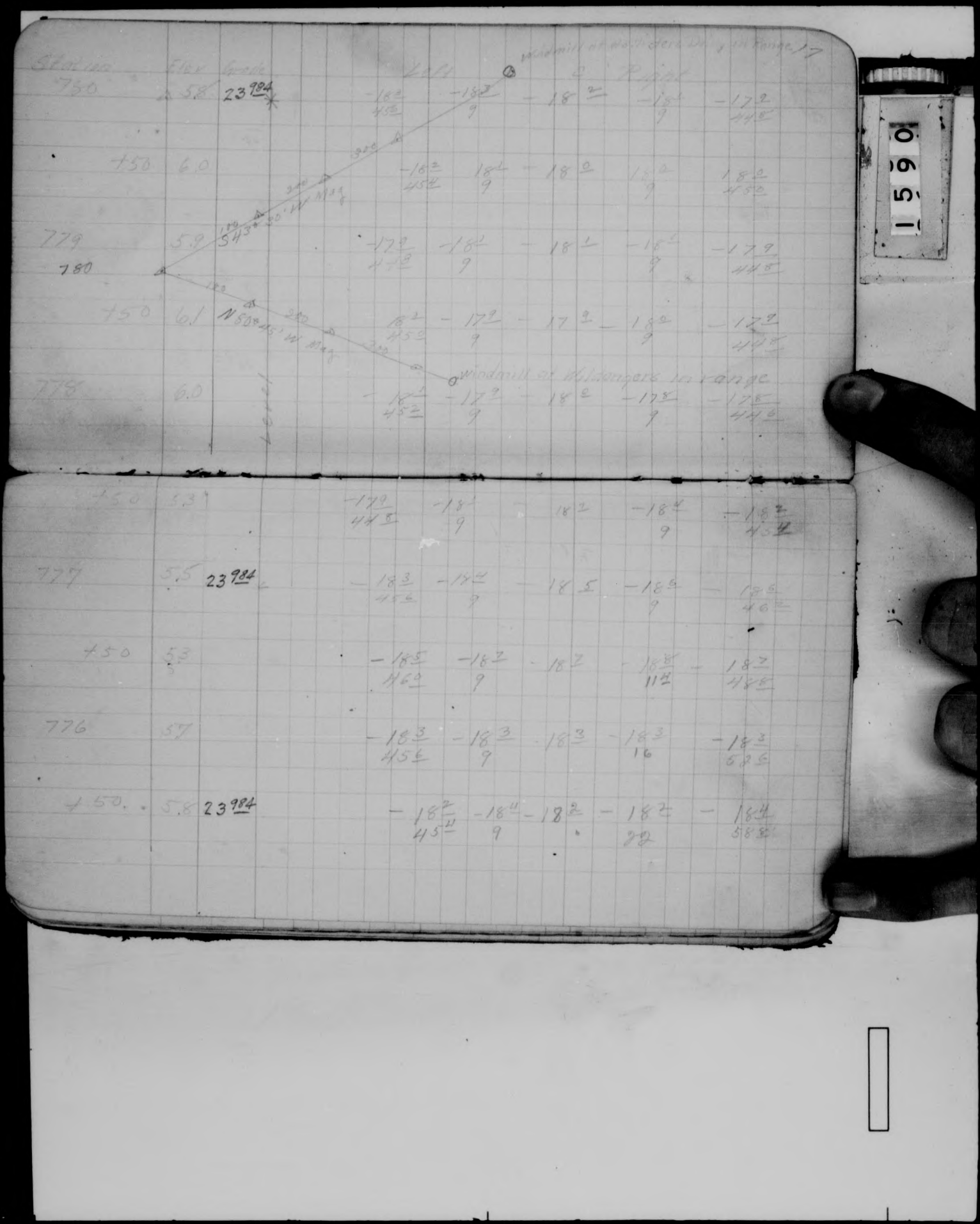
1587

Station	Elev. Grade		Left		C	Right		
770	7.3		$-16\frac{7}{42}$	$-16\frac{7}{9}$	$-16\frac{7}{}$	$-16\frac{7}{22}$	$-17\frac{0}{56}$	
750	7.3		$-16\frac{5}{42}$	$-16\frac{7}{9}$	$-16\frac{7}{}$	$-16\frac{8}{22}$	$-16\frac{8}{55}$	
+45	6.3							
+44	5.3							
+42	6.8							
B.M. Elev. 7.47	Hub by fence 150' Rt. Sta 769+39.							
+39	7.9							
+35	7.3				$16\frac{7}{}$			
769	7.7		$-16\frac{9}{42}$	$-16\frac{8}{9}$	$-16\frac{8}{}$	$-16\frac{9}{22}$	$-16\frac{8}{55}$	
150	7.5		$-16\frac{5}{42}$	$-16\frac{5}{9}$	$-16\frac{5}{}$	$-16\frac{3}{22}$	$-16\frac{5}{55}$	
768	7.7	23.984	$-16\frac{3}{41}$	$-16\frac{6}{9}$	$-16\frac{3}{}$	$-16\frac{7}{22}$	$-16\frac{6}{55}$	

1588

Station	Elev	Grade	Left		C	Right	
775	△ 5.0		$-18\frac{3}{45}$	$-18\frac{4}{9}$	$18\frac{3}{}$	$-18\frac{3}{22}$	$-18\frac{3}{58}$
+50	5.9		$18\frac{4}{45}$	$-18\frac{2}{9}$	$-18\frac{1}{}$	$-18\frac{3}{22}$	$-18\frac{2}{58}$
774	6.1		$-17\frac{6}{44}$	$-17\frac{2}{9}$	$-17\frac{9}{}$	$-18\frac{5}{22}$	$-18\frac{3}{58}$
+50	6.2		$-17\frac{8}{44}$	$-17\frac{8}{9}$	$-17\frac{8}{}$	$-17\frac{8}{22}$	$-17\frac{8}{57}$
773	6.6		$-17\frac{4}{43}$	$-17\frac{4}{9}$	$-17\frac{4}{}$	$-17\frac{3}{22}$	$-17\frac{3}{56}$
+50	6.7		$-17\frac{2}{43}$	$-17\frac{3}{9}$	$-17\frac{3}{}$	$-17\frac{3}{22}$	$-17\frac{5}{57}$
772	6.8		$-17\frac{2}{43}$	$-17\frac{3}{9}$	$-17\frac{2}{}$	$-17\frac{2}{22}$	$-17\frac{2}{56}$
+50	6.9		$-17\frac{1}{43}$	$-17\frac{1}{9}$	$-17\frac{1}{}$	$-17\frac{1}{22}$	$-17\frac{1}{56}$
771	7.2		$-16\frac{8}{42}$	$-16\frac{8}{9}$	$-16\frac{8}{}$	$-16\frac{8}{22}$	$-16\frac{8}{55}$
+50	7.4	23.98	$-16\frac{6}{42}$	$-16\frac{6}{9}$	$-16\frac{6}{}$	$-16\frac{6}{22}$	$-16\frac{6}{55}$

1589


Station
Elev
Grade
Point
windmill or windmakers in range
windmill or windmakers in range
1596

Station	Elev		Left			Right	
785	5.9	23952	$-18\frac{2}{45\frac{1}{2}}$	$-18\frac{2}{9}$	$-18\frac{0}{}$	$-18\frac{2}{9}$	$-18\frac{0}{45\frac{0}{}}$
750	5.9	23955	$-18\frac{5}{46\frac{0}{}}$	$-18\frac{3}{9}$	$-18\frac{2}{}$	$-18\frac{1}{9}$	$-18\frac{2}{45\frac{1}{2}}$
784	5.8	23958	$-18\frac{5}{46\frac{1}{}}$	$-18\frac{2}{9}$	$-18\frac{2}{}$	$-18\frac{2}{9}$	$-18\frac{2}{45\frac{1}{2}}$
750	5.6	23961	$-18\frac{2}{45\frac{1}{2}}$	$-18\frac{4}{9}$	$-18\frac{4}{}$	$-18\frac{2}{9}$	$-18\frac{3}{45\frac{0}{}}$
783	5.6	23964	$-19\frac{0}{47\frac{2}{}}$	$-18\frac{1}{42}$	$-18\frac{2}{9}$	$-18\frac{4}{}$	$-18\frac{3}{9}$ $-18\frac{3}{45\frac{0}{}}$
750	5.1	23967	$-18\frac{1}{45\frac{2}{}}$	$-18\frac{0}{9}$	$-18\frac{3}{}$	$-18\frac{2}{9}$	$-18\frac{1}{45\frac{1}{}}$
782	5.8	23971	$-17\frac{9}{44\frac{1}{}}$	$-18\frac{0}{9}$	$-18\frac{2}{}$	$-18\frac{2}{9}$	$-18\frac{1}{45\frac{1}{}}$
750	5.8	23974	$-18\frac{0}{45\frac{2}{}}$	$-18\frac{2}{9}$	$-18\frac{2}{}$	$-18\frac{2}{9}$	$-18\frac{2}{45\frac{1}{2}}$
781	5.9	23978	$-18\frac{2}{45\frac{1}{2}}$	$-18\frac{1}{9}$	$-18\frac{1}{}$	$-18\frac{0}{9}$	$-18\frac{0}{45\frac{0}{}}$
750	5.9	23981	$-18\frac{1}{45\frac{0}{}}$	$-18\frac{1}{9}$	$-18\frac{1}{}$	$-18\frac{0}{9}$	$-17\frac{9}{44\frac{1}{}}$

15911

Station	Fm						
720	4.6	23919	-193	-192	-193	-193	-193
			173	9	9	9	9
750	5.0	23922	-185	-185	-182	-185	-198
			9	9	9	9	9
754	5.3	23924	-198	-185	-184	-184	-184
			9	9	9	9	9
755	5.5	23929	194	-185	-184	-184	-184
			9	9	9	9	9
768	5.4	23932	-193	-184	-185	-183	-184
			9	9	9	9	9
750	5.2	23935	-184	-182	-182	-182	-182
			9	9	9	9	9
7867	5.0	13938	-182	-182	-182	-182	-182
			9	9	9	9	9
750	5.1	23941	-184	-182	-182	-182	-182
			9	9	9	9	9
7886	5.3	23945	-184	-184	-186	-184	-184
			9	9	9	9	9
751	5.6	23949	-182	-183	-184	-184	-184
			9	9	9	9	9

1592

Station	Sag Scale		Left			C	Right		
+78	4.4		149 / 388	154 / 35	+165 / 9	−19 5	205 / 9	207 / 502	
+50	2.4	23895	−188 / 462	−207 / 30	−214 / 9	−21 5	−216 / 9	−205 / 25	−184 / 34	−185 / 462
+31	3.4		−205 / 582	−212 / 24	−217 / 9	−20 5	−192 / 3	−188 / 8	−185 / 9	−185 / 460
+27	5.3		−216 / 512	−216 / 29	−204 / 9	−200 / 4	−186	+184 / 9	−184 / 458	
793	4.9	23899	−215 / 520	−207 / 41	−192 / 36	+190 / 7	−190	+189 / 9	−192 / 470	
+50	4.5	23902		−193 / 476	−193 / 9	−19 4	−192 / 9	−192 / 474	
792	4.3	23906		−195 / 492	−197 / 9	−19 6	−195 / 9	−195 / 480	
+50	4.4	23909		−196 / 482	−196 / 9	−19 5	−195 / 9	−195 / 489	
791	4.5	23912		−195 / 486	−195 / 9	−19 4	+194 / 9	−194 / 476	
+50	4.6	23915		−195 / 462	−193 / 9	−19 3	−194 / 9	−195 / 482	

1593

D

Sta	Elev	Grade
750	5.3	23876
796	5.3	23879
785	5.3	
750	4.3	
750	3.5	23882
795	1.9	23886
770	3.3	
750	6.9	23889
718	11.4	
794	7.9	23892

-19² +18⁵ - 18⁶ -18⁴ -17²
47⁴ 9 44²

-19² -18⁵ - 18⁶ -18⁵ -18⁴
47⁰ 9 9 45⁴

- 18⁶

-19¹ - 19⁶

-20² -20⁵ - 20⁴ -19² - 20²
49⁴ 9 9 50⁴

-20² -21⁸ - 21⁶ -21⁸ -20² -18⁶
50⁴ 9 9 35² 46²

- 20⁶

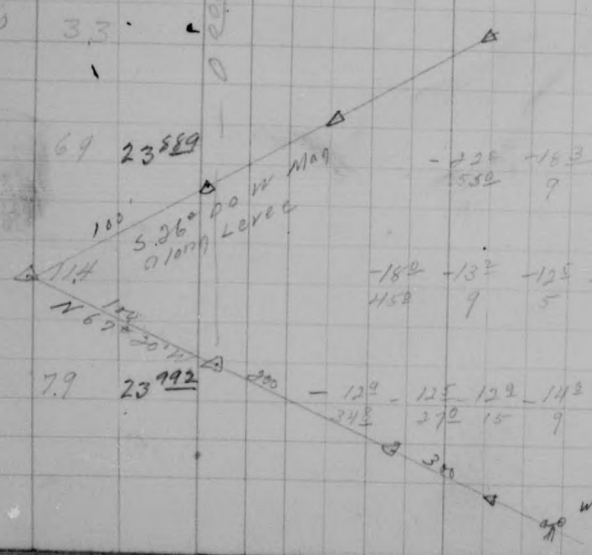
-22⁸ +16³ - 17⁰ +15⁸ - 18⁰
55⁸ 9 9 35⁰

-18⁰ +13² +12⁵ - 12⁵ 13³ - 16⁵
45⁹ 9 5 9 46⁰

- 12⁹ - 12⁵ 12⁹ - 14³ - 16⁰ -16⁸ 20²
34⁵ 27⁰ 15 9 9 49⁴

94

1594



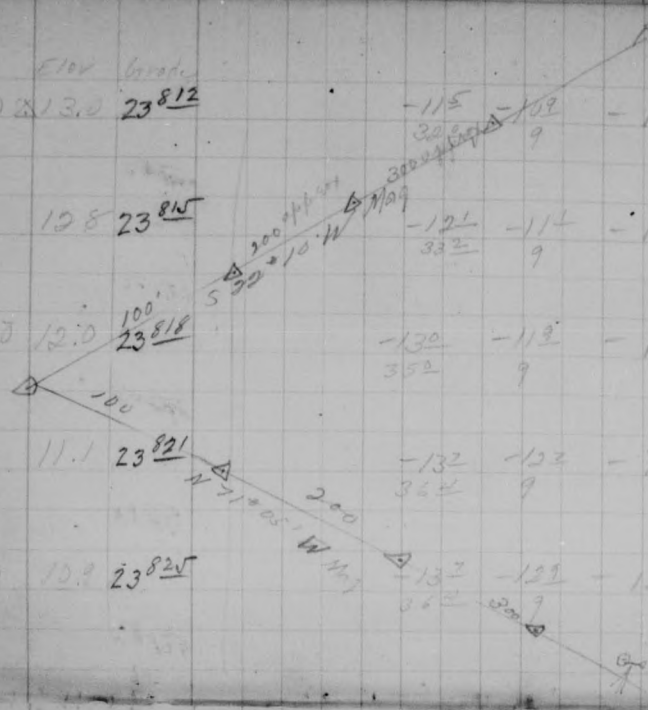
D

	Elev. Grade						
750	98	23844	-15 2/37 2	-14 3/9	-14 0	-13 6/9	-13 4/35 2
801	95	23847	-15 6/43 2	-14 5/9	-14 3	-13 9/9	-13 3/35 5
750	88	23857	-16 2/41 2	-15 4/9	-15 0	-14 7/9	-14 1/37 2
800	84	23854	-16 6/42 2	-15 8/9	-15 4	-15 3/9	-14 8/38 6
758	75	23867	-17 2/44 4	-16 6/9	-16 4	-16 1/9	-15 5/40 2
799	69	23860	-18 4/45 2	-17 3/9	-17 0	-16 7/9	-16 2/41 2
750	67	23863	-18 2/45 4	-17 4/9	-17 1	-16 9/9	-16 2/41 3
798	63	23866	-18 5/46 2	-17 7/9	-17 4	-17 5/9	-16 4/41 8
750	56	23869	-19 1/47 2	-18 5/9	-18 3	-17 7/9	-16 9/42 8
797	53	23872	-19 2/47 3	-18 6/9	-18 6	-18 3/9	-17 5/44 0

D-2

1595

15961



	Elev	Grade					
450	13.0	23 812	-115 32	-102 9	-108	-102 9	-104 298
806	12.8	23 815	-121 332	-114 9	-110	-107 9	-107 304
450	12.0	23 818	-130 352	-119 9	-118	-117 9	-113 316
806 450							
805	11.1	23 821	-132 364	-123 9	-127	-123 9	-120 330
450	12.9	23 82V	-137 362	-129 9	-129	-126 9	-124 338
804	10.9	23 829	-129 368	-129 9	-129	-126 9	-123 336
450	10.9	23 831	-141 377	-131 9	-129	-125 9	-123 335
803	10.5	23 834	-140 370	-130 9	-130	-122 9	-124 338
450	10.7	23 837	-1119 370	-133 9	-131	-132 9	127 347
802	10.3	23 841	-145 38	-135 9	-135	-133 9	-127 344

D

		Elev Grade							
+50	7.4	23779		16 6/42 2	-16 3/9	-16 4/9	-16 4/9	-16 7/43 4	
811	7.8	23782		-15 8/40 2	-15 9/9	-16 0/9	-16 2/9	16 0/41 0	
+50	8.3	23786		-13 5/44 2	-15 5/9	-15 5/9	-15 5/9	-15 8/40 6	
810	8.6	23789		-15 2/37 4	-15 0/9	-15 2/9	-15 2/9	-15 4/39 8	
+50	9.2	23792		-14 5/38 2	-14 6/9	-14 6/9	-14 6/9	-14 9/38 8	
809	9.6	23795		-14 4/37 2	-14 2/9	-14 2/9	-14 3/9	-14 3/38 5	
+50	10.5	23798		13 2/33 4	-13 3/9	-13 3/9	-13 3/9	-13 5/36 2	
808	11.3	23801		-12 3/33 2	-12 5/9	-12 5/9	-12 5/9	13 0/35 2	
+50	12.5	23804		-11 6/32 4	-11 5/9	-11 3/9	-11 3/9	-11 6/32 2	
807	13.0	23808		-11 3/31 6	-10 3/9	-10 5/9	-10 5/9	-10 5/30 2	

1597

D

	Elev.	Grade					
750	6.6	23 747	-16 4 / 415	-16 9 / 9	-17 1	-17 2 / 9	-17 4 / 438
816	6.8	23 750	-16 5 / 420	-16 9 / 9	-16 9	-17 0 / 9	-17 2 / 436
750	6.6	23 753	-16 4 / 418	-16 6 / 9	-17 1	-17 1 / 9	-17 3 / 436
815	6.3	23 657	-16 2 / 428	-17 3 / 9	-17 5	-17 6 / 9	-17 9 / 448
750	6.6	23 760	-17 2 / 434	-17 2 / 9	-17 2	-17 5 / 9	-17 8 / 446
814	6.2	23 763	-17 4 / 438	-17 5 / 9	-17 6	-17 6 / 9	-17 6 / 442
750	6.2	23 766	-17 4 / 438	-17 5 / 9	-17 6	-17 6 / 9	-17 9 / 448
813	6.7	23 769	-17 2 / 434	-17 3 / 9	-17 1	-16 9 / 9	-17 6 / 442
750	6.6	23 773	-17 2 / 434	-17 2 / 9	-17 2	-17 2 / 9	-17 2 / 434
812	7.2	23 776	-16 7 / 424	-16 4 / 9	-16 4	-16 6 / 9	-16 8 / 426

1598

D

	Elev	Grade					
750	4.6	23 7 14	-19 4 / 47 2	-19 4 / 9	-19 4	-19 4 / 9	-19 4 / 47 2
821	4.9	23 7 18	-18 5 / 46 4	-18 9 / 9	-18 8	-18 7 / 9	-18 5 / 46 2
750	5.2	23 7 21	-18 5 / 45 0	-18 5 / 9	-18 5	-18 2 / 9	-18 6 / 46 2
820 A	6.0	23 7 24	-17 7 / 44 4	-17 9 / 9	-17 7	-17 7 / 9	-17 6 / 44 2
750	6.2	23 7 27	-17 6 / 44 2	-17 5 / 9	-17 5	-17 5 / 9	-17 4 / 43 8
819	6.6	23 7 31	17 0 / 43 2	+16 9 / 9	-17 1	-17 1 / 9	17 2 / 43 4
750	6.5	23 7 34	-17 1 / 43 2	-17 2 / 9	-17 2	-17 2 / 9	-17 0 / 43 0
818	6.1	23 7 37	-17 3 / 43 6	-17 3 / 9	-17 3	-17 3 / 9	-17 2 / 43 4
750	6.4	23 7 40	-17 3 / 43 6	-17 2 / 9	-17 3	-17 2 / 9	-17 2 / 43 4
817	6.6	23 7 44	-17 0 / 43 0	-17 0 / 9	-17 1	-17 1 / 9	-17 3 / 43 6

15996

D

Elev	Grade							
750	2,10	23612						
826								
	2,12	23685						
750	2,8	23658						
825								
	32	23791						
750	8,2	23794						
750	4,10	23708						
822								
	4,4	23711						

1600

D

	Elev	Grade					
750	0.9	23 649	22 1/2 53 2	22 1/2 9	22 5	22 1/2 9	22 1/2 53 2
831	1.1	23 653	22 1/2 53 2	22 1/2 9	22 1/2	22 1/2 9	22 1/2 53 2
750	1.0	23 656	22 1/2 53 2	22 0 9	22 1/2	22 1/2 9	22 1/2 53 2
830	1.1	23 659	22 3/4 53 2	21 8/9	22 1	22 0/9	21 7/9 52 4
750	2.0	23 663	22 1/2 53 2	21 8/9	21 7	22 0/9	21 8/9 52 8
829	1.9	23 666	22 2/9 53 2	21 8/9	21 7	21 8/9	21 6/9 52 2
750	1.9	23 669	22 0 53 0	21 8/9	21 8	21 8/9	21 8/9 52 6
828	1.8	23 672	21 9/9 52 8	21 8/9	21 8	21 9/9	22 0 53 0
750	1.7	23 675	22 0 53 0	22 0/9	22 0	22 0/9	22 0 53 0
827	2.2	23 679	21 8/9 52 8	21 5/9	21 5	21 5/9	21 4/9 53 2

28

11091

0 0063

D	Elev	Grade					
T50	-1.3	23617		24⅚ / 58½	24⅝ / 9	24⅜ / 9	24⅛ / 58½
836	-0.8	23620		24⅝ / 58½	24⅝ / 9	24⅜ / 9	24⅛ / 58½
+50	-1.0	23623		24⅝ / 58½	24⅝ / 9	24⅜ / 9	24⅛ / 58½
835	-0.9	23627		24⅜ / 58½	24⅛ / 9	24⅝ / 9	24⅛ / 58½
+50	-0.7	23630		24⅜ / 58½	24⅛ / 9	24⅜ / 9	24⅛ / 58½
834	1.4	23633		24⅛ / 58½	24⅛ / 9	24⅜ / 9	24⅛ / 58½
+50	-0.3	23636		24⅜ / 58½	24⅛ / 9	24⅜ / 9	24⅛ / 58½
833	1.2	23640		24⅛ / 58½	24⅛ / 9	24⅜ / 9	24⅛ / 58½
+603 △1							
+50	1.2	23643		24⅝ / 58½	24⅛ / 9	24⅜ / 9	24⅛ / 58½
832	-0.2	23646		24⅛ / 58½	24⅛ / 9	24⅜ / 9	24⅛ / 58½

Oct 10 1907

1902

+20	1.0		-22.1 (53.2)	-22.1 (9)	-22.5	-22.1 (9)	-22.1 (53.2)
841	-1.0	23.588	-22.1 (53.2)	-23.0 (9)	-24.0	-23.2 (9)	-22.1 (53.2)
+50	-0.3	23.591	23.7 (56.4)	-23.2 (9)	-23.2	-23.2 (9)	22.5 (53.2)
Oct 11 1927							
840	-0.4	23.594	-23.4 (55.8)	-24.2 (9)	-24.0	-24.2 (9)	-22.1 (53.2)
+50	-0.4	23.597	-22.1 (53.2)	-24.0 (9)	-24.0	-24.0 (9)	-22.1 (53.2)
839	-0.4	23.601	-24.5 (58.2)	-24.0 (9)	-24.0	-24.0 (9)	-22.1 (53.2)
+50	-1.0	23.604	-24.3 (57.6)	-24.5 (9)	-24.6	-24.6 (9)	-22.1 (53.2)
838	-1.3	23.607	-24.4 (57.6)	-24.9 (9)	-24.8	-24.2 (9)	-24.5 (58.0)
+50	-1.4	23.610	-25.1 (59.2)	-25.2 (9)	-25.0	-25.0 (9)	-24.6 (58.2)
837	-1.2	23.614	-24.6 (58.2)	-24.6 (9)	-24.6	-24.6 (9)	-25.0 (59.0)

1903

D	Elev Corr						
846	-3.2	23 555	26 4/62	26 7/9	26 8	26 8/9	26 8/62 6
+50	-3.4	23 558	26 8/62 6	27 0/9	27 0	27 0/9	26 9/62 8
845	-3.6	23 562	26 9/62 8	-27 1/9	-27 2	-27 2/9	27 1/63 2
+50	-3.8	23 565	-27 2/63 4	-27 2/9	-27 2	-27 2/9	-27 2/63 4
844	-3.6	23 568	-27 2/63 4	-27 2/9	-27 2	-27 2/9	-27 2/63 4
+50	-3.6	23 571	-27 2/63 2	-27 2/9	-27 2	-27 2/9	-27 1/63 4
843	-3.5	23 575	-26 9/62 8	-27 0/9	-27 1	-27 2/9	-27 2/63 4
+50	-3.0	23 578	-26 1/61 2	-26 6/9	-26 6	-26 6/9	-26 5/62 6
842	-2.3	23 581	-23 7/56 4	-25 8/9	-25 8	-25 8/9	-22 8/54 6
+50	-1.2	23 584	-22 1/53 2	-22 2/9	-21 8	-22 2/9	-22 1/52 2
+22 3 Δ							

1604

1605

1606

D	Elev Grade					
861	-3.5	23 463	-26 2/6 1/2	-26 8/9	-26 8/9	-26 6/6 2/2
+50	-4.1	23 461	-27 1/6 3/2	-27 4/9	-27 5/9	-27 3/6 3/6
860	-4.5	23 464	-27 4/6 3/6	-27 5/9	-27 2/9	-26 8/6 2/6
+50	-4.3	23 467	-27 3/6 3/6	-27 5/9	-27 7/9	-27 4/6 3/6
859	-4.6	23 471	-27 4/6 3/6	-27 8/9	-28 1/9	-27 6/6 3/6
+50	-4.4	23 474	-27 4/6 3/6	-27 7/9	-27 2/9	-27 4/6 3/6
858	-4.4	23 477	-27 6/6 4/2	-27 8/9	-27 7/9	-27 4/6 3/6
+50	-4.3	23 480	-27 4/6 3/6	-27 6/9	-27 8/9	-27 7/6 4/4
857	-4.4	23 484	-27 7/6 4/4	-27 8/9	-27 7/9	-27 8/6 4/6
+50	-4.3	23 487	-27 7/6 4/4	-27 8/9	-27 7/9	-27 6/6 4/2

1091

D	Elev.	Grade					
866	-3.4	23 435	26 7/624	26 8/9	26 8	26 1/9	25 9/608
+50	-3.3	23 428	26 2/614	26 5/9	26 7	26 4/9	25 9/608
Oct 16 / 1907.							
865	-3.1	23 431	26 9/625	26 5/9	26 5	26 3/9	25 9/608
+50	-2.7	23 435	26 5/622	26 1/9	26 1	26 1/9	25 6/602
864	-2.4	23 438	25 5/620	25 5/9	25 8	25 6/9	24 5/580
+50	-1.7	23 442	26 2/614	25 2/9	25 1	25 1/9	22 3/536
863	1.3	23 445	25 9/605	20 5/9	22 1	20 9/9	20 0/530
+815 △							
+50	0.9	23 448	24 2/612	22 5/9	22 5	22 2/9	20 0/530
862	-2.3	23 451	26 2/624	25 2/9	25 0	23 3/9	20 0/530
+50	-3.2	23 455	26 9/629	26 6/9	26 6	26 5/9	26 3/614

1608

D.	Elev	Grade
871	-4.6	23393
+50	-4.6	23396
870	-4.5	23399
+50	-4.2	23402
869	-4.2	23406
+50	-4.0	23409
868	-4.1	23412
+50	-3.8	23416
867	-3.8	23419
+50	-3.3	23422

6091

D

Elev Form

876 -33 23 340

450 -35 23 344

875 -35 23 342

450 -36 23 320

874 -36 23 323

450 -12 23 377

873 -34 23 380

450 -35 23 383

872 -39 23 326

450 -41 23 320

1610

1611

D	Elev	Grade						
886	-0.9	23 306						
750	-1.3	23 308						
885	-1.7	23 311						
750	-1.9	23 313						
884	-2.8	23 315						
750	-2.9	23 317						
883	-2.2	23 320						
750	-2.5	23 322						
Oct. 17 1907								
882	-2.6	23 324						
750	-0.3	23 326						
1234 △								

1911

D	Elev	Grad					
891	-0.5	23284	21[5]/524	-23[8]/9	-23[8]/9	-23[5]/9	-23[2]/528
+50	1.3	23286	-23[9]/568	-23[4]/9	-23[2]/9	-21[5]/9	-21[5]/524
890	1.6	23289	-22[3]/572	-21[7]/9	-21[7]/9	-21[5]/9	-21[0]/510
+50	1.7	23287	-23[5]/560	-21[6]/9	-21[5]/9	-21[3]/9	-21[2]/514
889	2.3	23292	-22[2]/574	-21[2]/9	-21[0]/9	-21[0]/9	-21[0]/510
+50	1.8	23294	-22[6]/582	-21[8]/9	-21[8]/9	-21[5]/9	-21[0]/510
8.88	0.7	23297	-22[7]/584	-22[2]/9	-22[0]/9	-21[2]/9	-21[0]/510
+50	1.1	23299	-22[2]/588	-22[2]/9	-22[0]/9	-20[2]/9	-21[0]/510
887	0.2	23302	-23[2]/594	-23[2]/9	-23[1]/9	-23[1]/9	-21[5]/522
+50	0.3	23304	-22[5]/586	-23[2]/9	-23[0]/9	-22[5]/9	-21[5]/520

-0.0045

16113

D	Elev	Grade						
150	0.8	23264	236 / 562		235 / 9	24	235 / 9	235 / 560
895	-0.5	23266	232 / 554		232 / 9	23	235 / 9	237 / 561
150	0.1	23268	233 / 556		232 / 9	23	231 / 9	234 / 552
894	0.1	23271	239 / 558		231 / 9	23	232 / 9	236 / 562
175	1.7	23272		215 / 520	215 / 9	21	215 / 9	235 / 562
150	-0.7	23273	235 / 562		238 / 9	23	235 / 9	235 / 561
893	-0.5	23276	235 / 560		237 / 9	23	237 / 9	234 / 552
150	-0.4	23278	237 / 564		236 / 9	23	236 / 9	236 / 562
892	-0.1	23280	236 / 562		234 / 9	23	234 / 9	234 / 561
150	-0.1	23282	235 / 562		234 / 9	23	234 / 9	237 / 558

-0.0045

1914

| D | Elev. Grade | | |

D

Elev Grade

750 4.9

905 5.1 23.226

750 4.8

Pages 42 To 43 Used In
Final Estimate No. 156

Embankment Original Cross Sections Continued

081 △ in Original Cross Section Book No 7, page 3.

904 4.3 23.226

750 3.9 23.228

903 3.5 23.231

750 3.5 23.233

902 3.6 23.235

750 3.6 23.237

901 3.8 23.240

1911

D	Elev	Grade	
+50	5.4		
910	△	5.4	
+50	5.4		
909		5.1	23.2035
+50	5.1		
908		5.1	23.202
+50	5.1		
907		4.9	23.225
B.M. Elev. 6.163			350' Rt. D 906+50 Hub on E. side fence post
+50	5.2		
906	△	5.0	23.217

1911

D	Elev Grade
750	416
915	414
750	417
914	412
750	416
913	461
750	418
912	412
750	511
911	554

1618

730	7.7	
916	5.6	
758	4.8	
751	0.8	
750	-2.6	

733	-0.7	
1282	5.7	
917	6.9	
750	5.3	
916	11.6	

1619

D Thu Grade

923 553

924 550

921 449

920 449

919 448

550 650

1620

D	Elev Grade
928	5.6
750	6.0
927	6.0
750	6.0
926	6.1
750	6.2
925	6.2
750	6.0
924	5.7
750	5.4

1621

1185	3.4	
1150	2.6	
1143	2.1	
930	0.0	
1150	1.6	
1171	2.9	
1170	4.8	
1152	5.2	
1229	5.6	
1150	5.8	

1622

935 4,2

450 3,9

431∧ 34

934

450 3,6

933 4,1

450 4,4

932 5,0

450 1,6

931 1,8

1623

1624

August 5, 1909

Sta.	Elev.	Grade		Lt		C.		Rt	
# 747+0.8 Δ 17½ Rt									
D 747 + 8.8 Δ on 0°30'	15.2	23.94	Flag Pole on Basement Wall	-1.0 / 5.6	-2.3 / 9.0	-2.8	-13.4 / 9.0	-15.0 / 15.0	-16.0 / 30.0	-16.1 / 41.2
747	14.9			-1.1 / 10.7	-2.1 / 9.0	-2.1	-13.9 / 9.0	-15.2 / 20.0	-16.3 / 30.0	-17.0 / 43.0
+ 76 E Δ E.C.	14.4			-1.4 / 11.4	-2.6 / 9.0	-2.6	-13.4 / 9.0	-16.1 / 20.0	-17.1 / 43.2
+50	11.5			-2.8 / 13.2	-6.0 / 9.0	-12.5	-14.9 / 5.0	-17.1 / 20.0	-18.4 / 45.8
746	8.5		Steeple on Church	-5.8 / 17.7	-12.6 / 10.0	-12.0 / 9.0	-16.5	-17.9 / 9.0	-19.2 / 30.0	-19.1 / 47.2
+50	5.1			-13.2 / 37.0	-15.8 / 17.0	-17.7 / 9.0	-18.9	-19.6 / 9.0	-19.1 / 47.2
745	4.9			-17.2 / 37.5	-18.9 / 9.0	-19.1	-19.3 / 9.0	-19.1 / 47.2
+50	4.0			-17.9 / 35.9	-19.4 / 9.0	-20.0	-20.0 / 9.0	-19.9 / 47.4
744	3.7			-20.4 / 37.9	-20.9 / 9.0	-20.3	-20.8 / 9.0	-20.4 / 42.8
+50	3.8			-17.8 / 38.7	-19.0 / 32.0	-20.2 / 9.0	-20.2	-20.0 / 9.0	-19.8 / 41.8

Sta	Elev.	Grade	L	C	R
		33.9+2			
H 740 +63E	3.2		-15.4 -16.5 -16.7 -16.3 -20.8 -20.1 30.1 27.0 21.0 9.0 9.0		
+93E ΔCC	3.0	10°20 Rt.	-18.5 -18.6 -20.8 -21.0 -20.6 -19.8 36.8 27.0 9.0 9.0		
741	2.8		-18.2 -19.0 -20.9 -21.2 -20.7 -19.8 36.8 34.0 9.0 9.0		
+50	3.8		-20.2 -20.4 -20.2 -20.1 -18.1 -16.9 28.8 9.0 9.0 39.0 42.2		
742	5.4		-19.6 -19.0 -18.6 -18.3 -16.2 -11.5 38.8 9.0 9.0 18.0 32.0		
+ 26.			-16.6 -18.6 -18.3 -15.7 -11.1 -11.1 36.9 9.0 9.0 18.0 31.2		
+50 Δ Δ 13.8			-18.9 -18.8 -13.4 -10.7 -10.4 -11.0 -12.5 37.4 29.0 9.0 9.0 24.0 42.0		
+75			-9.1 -9.4 -8.6 -8.8 -11.5 -18.0 -18.0 28.7 9.0 3.0 9.0 36.0 45.0		
743	9.8	High tower	-10.2 -12.0 -14.2 -14.7 -13.5 -13.4 24.3 9.0 3.0 9.0 47.8		
743 +20			-11.8 -13.6 -15.2 -14.7 -15.7 -19.7 36.0 20.0 9.0 9.0 48.4		

1625

1626

Level

Level

1627

Sta	Elev.	Grade 28.98						
727+50			-14.7 31.2	-14.8 16.0	-14.8 9.0	-12.7	-17.6 9.0	-9.9 28.8
728	6.0		-15.1 31.7	-14.0 16.0	-17.2 9.0	-18.0	-17.6 9.0	-9.7 29.2
+50	6.0	Level	-14.0 31.9	-15.2 16.0	-17.6 9.0	-18.8	-17.8 9.0	-10.3 28.4
729	6.1		-15.2 31.5	-14.7 15.0	-12.9 9.0	-17.9	-12.7 9.0	-9.8 28.5
+50	6.1		-14.9 31.2	-14.7 12.0	-16.9 9.0	-17.9	-17.8 9.0	-9.8 28.2
730	7.0		-14.4 30.6	-15.1 15.0	-16.4 9.0	-17.0	-16.9 9.0	-9.5 28.0
+50	9.1		-14.6 30.9	-14.9 16.0	-16.7 9.0	-16.9	-17.1 9.0	-9.5 28.0
731	6.7		-15.0 32.0	-14.8 14.0	-16.7 9.0	-17.3 7.0	-17.3 9.0	-9.0 27.0
+50	6.7	Level	-15.2 32.0	-16.2 16.0	-16.5 9.0	-17.2 7.0	-17.9 9.0	-9.2 27.4
732	6.9		-15.2 32.1	-14.8 12.5	-16.4 9.0	-17.3 6.0	-17.1 9.0	-9.4 27.8

1628

Level

Level

1629

Sta.	Elev. Grade	H	C	B.M.
	23.984			
718	11.0	-15.2 / 28.8	-15.2 / 90	-15.0
		-13.9 / 90	-12.8 / 27.5	-11.6 / 32.2
+50	10.1	-14.0 / 90.0	-14.0 / 9.0	-13.9
		-14.1 / 9.0	-13.9 / 19.0	-10.0 / 37.0
+91	8.9	-14.6 / 30.9	-14.5 / 9.0	-15.1
		-15.2 / 7.0	-16.2 / 13.0	-10.6 / 23.0
		-11.0 / 29.5	-12.9 / 37.0	
719 +31	8.0	-14.8 / 31.8	-15.3 / 9.0	-15.8 / 23.0
		-16.0 / 9.0	-16.1 / 11.5	-15.7 / 20.0
		-11.3 / 28.0	-10.9 / 40.6	
+51	7.1	-13.4 / 32.1	-16.1 / 9.0	-14.0 / 33.5
		16.7 / 9.0	-16.9 / 6.5	-16.5 / 9.0
		-15.8 / 16.0	-14.7 / 20.5	-13.8 / 26.0
		-10.9 / 39.0	-11.1 / 39.8	
720	6.5	-20.5 / 33.3	-15.2 / 30.0	-17.0 / 20.0
		-17.2 / 9.0	-17.5	-17.9 / 9.0
		-14.8 / 9.0	-14.9 / 20.0	-10.6 / 21.0
		-11.0 / 35.0	-11.7 / 39.0	
+50	6.7	-16.4 / 33.4	-16.2 / 30.0	-17.5 / 20.0
		-17.8 / 9.0	-17.9	-16.7 / 9.0
		-14.9 / 9.0	-12.4 / 18.0	-11.7 / 20.0
		-10.9 / 29.0	-10.6 / 39.0	
721	6.4	-19.2 / 31.8	-19.1 / 30.0	-19.1 / 20.0
		-18.3 / 8.0	-17.6	-16.8 / 9.0
		-15.3 / 13.0	-13.4 / 20.0	-12.9 / 30.0
		-14.5 / 39.0		
+60	5.9	-19.8 / 38.1	-20.3 / 30.0	-20.6 / 20.0
		-20.1 / 9.0	-18.6 / 30.0	-18.1
		-16.7 / 9.0	-14.9 / 20.0	-12.1 / 30.0
		-12.2 / 30.0	-13.3 / 40.0	-16.9 / 42.8
722	6.3	-19.5 / 38.9	-19.4 / 30.0	-19.6 / 20.0
		-20.1 / 9.0	-18.0 / 4.0	-17.7
		-16.9 / 3.0	-14.3 / 9.0	-13.0 / 15.0
		-12.0 / 24.0	-13.4 / 25.0	-14.3 / 30.0
		-18.9 / 40.0	-16.7 / 42.4	

Lorel

Fill Grade

Sta 0

Sta 2

Lorel

Sta 0 at Barn on the Wm Johnston Farm

Fill Grade

Edge of Wm H. Johnston Home

1630

Sta.	Elev. Grade	Lt.	℄			Rt.
H 713	12.2 22584		-11.9 / 26.9	-11.8 / 9.0	-11.8	-11.7 / 9.0	-10.8 / 30.2
+50	12.2		-12.2 / 27.9	-11.9 / 9.0	-11.8	-11.7 / 9.0	-11.7 / 32.4
714	11.4		-12.5 / 27.8	-12.5 / 9.0	-12.6	-12.7 / 9.0	-12.4 / 23.9
+50	11.6	Level	-12.6 / 37.9	-12.5 / 9.0	-12.4	-12.1 / 9.0	-12.0 / 35.0
715	11.7		-12.5 / 27.8	-12.6 / 9.0	-12.6	-13.1 / 9.0	-12.0 / 35.0

No. 1 on 1st station
B.M.

+50	11.2		-12.9 / 38.4	-13.0 / 9.0	-12.8	-12.6 / 9.0	-12.6 / 34.2
+51.9	center of road					
716	10.7		-12.9 / 38.4	-13.1 / 9.0	-13.8	-13.2 / 9.0	-12.8 / 34.4
+50	11.4	Level	-12.9 / 38.4	-12.6 / 9.0	-12.6	-12.7 / 9.0	-12.6 / 34.2
717	11.3		-12.4 / 27.6	-12.5 / 9.0	-12.7	-12.7 / 9.0	-12.3 / 34.8
717 +50	11.0		-12.9 / 38.4	-12.9 / 9.0	-13.0	-12.6 / 9.0	-13.1 / 35.2

100' 100' 100'

H 710+37 B.B.

58

27

1631

Sta.	Inter.	Grade	Rt				C		Lt	
H 709		19.0	11.4 / 26.1	11.1 / 20.0	10.4 / 14.0	8.9 / 9.0	-5.0	-0.8 / 9.0	-0.4 / 9.8	
	+50	21.1	-10.5 / 21.9	-10.5 / 20.0	-6.8 / 9.0	-2.9	-0.0 / 6.2	+0.6 / 9.0	+2.5 / 9.5	
710		18.3	-11.2 / 26.6	-10.5 / 20.0	-8.7 / 9.0	-6.7	-0.0 / 9.0			
	+37.2	19.6	B.C. T.S.		10.6 / 29.9	-10.1 / 20.0	-7.9 / 9.0	-4.4	0.0 / 6.1	+2.1 / 9.0	+2.1 / 11.1
	+69.7	21.2			11.4 / 26.1	-11.1 / 18.0	-8.6 / 9.0	-3.9	-0.0 / 7	+1.2 / 9.0	+1.0 / 10.0
	+92.7	19.2	B.C. 7°30'LT								
711		19.3	-11.6 / 26.4	11.3 / 20.0	-9.6 / 9.0	-4.7	-0.3 / 9.0	-0.1 / 9.2		
	+50	15.0	-11.3 / 26.0	-11.1 / 9.0	-10.6 / 3.0	-7.0	-4.1 / 9.0	-0.1 / 18.2		
712		12.7	outside of wash-stock		-11.6 / 26.7	-11.6 / 9.0	-11.3	-12.2 / 5.0	-8.5 / 7.0	-2.0 / 17.0	
712+50		12.2			-11.7 / 26.6	-11.8 / 9.0	-11.8	-11.6 / 9.0	-10.6 / 16.3	-9.4 / 20.0	-7.7 / 21.0

1632

16133

Sta	Elev	Grade 22.99?						
704+60								
705	+60	△						
706		17.6		-10.7 / 26.1	-10.5 / 40.0	-8.9 / 9.0	-6.4	-4.5 / 7.0	-8.4 / 15.9
	+10	△ 17.5		-9.4 / 23.1	-9.1 / 30.0	-7.7 / 9.0	-6.5	-5.5 / 9.0	-4.4 / 17.8
	+60	18.7			-9.6 / 17.0	-7.9 / 9.0	-6.9	-5.0 / 9.0	-4.8 / 14.0	-4.2 / 17.0
707		16.5		-9.8 / 23.9	-9.6 / 30.0	-8.8 / 9.0	-7.5	-6.8 / 9.0	-4.8 / 18.0	
	+60	17.6		-10.3 / 24.6	-9.8 / 30.0	-7.7 / 9.0	-6.4	-4.7 / 9.0	-3.5 / 18.0	-1.7 / 11.2
708		21.1		-10.3 / 27.4	-11.4 / 30.0	-7.0 / 9.4	-2.9	-0.6 / 9.0	-0.5 / 10.0	
708	+60	19.5		-11.8 / 26.9	-11.9 / 30.0	-9.6 / 9.0	-4.6	-0.6 / 9.0	-0.6 / 10.2	

Level

Rod reading on face past

Rod reading on face past

Rod reading on face past

Note in line with ends of steel

Rod reading on face past

61

Road Crossing Rt of H716 +51.2

H716+51.2 = 0+00	90°0.0 Rt 35.6	Lt	C	Rt
0+9°		-1.6 / 14.4 -1.6 / 12.0	-1.6	-1.6 / 10.0 -1.6 / 14.4
0+84		-14.4 / 33.6 -14.3 / 12.0	-14.2	
0+50		-14.2 / 33.3 -14.6 / 12.0	-14.0	
1+00		-12.1 / 30.3 -13.0 / 12.0	-13.4	
1+29.6		-12.6 / 30.3 -12.4 / 12.0	12.3	
1+50.		-7.5 / 23.8 -8.0 / 12.0	-9.8	
1+70.		-2.4 / 15.6 -2.2 / 12.0	-1.5	
		-.27 / 13.1 -.05 / 12.0	-0.0	

Level

Grade changed
See H716 +42

1634

1635

Road Crossing at # 706+19.05 △ 66° 4'

# 706+19.05	26.660					
6+20.0	66° 4' 11"	-9.1 / 16.9	-9.1 / 12.0	-1.8	-1.3 / 12.0	-1.3 / 14.0
5+00	26.584	-5.5 / 20.0	-6.3 / 12.0	-3.6	-1.7 / 12.0	-1.4 / 11.1
4+50	23.724	-10.6 / 21.9	-9.2 / 12.0	-5.8	-2.9 / 12.0	-3.1 / 16.7
4+70	22.324	-9.6 / 24.4	-9.6 / 12.0	-6.7	-8.8 / 12.0	-8.7 / 20.4
4+00	20.224	-8.2 / 24.3	-7.7 / 12.0	-7.8	-2.5 / 12.0	-3.2 / 35.2
1+50	16.724	-5.0 / 19.5	-4.8 / 12.0	-4.8	-4.5 / 12.0	-4.6 / 19.3
2+00	12.224	-1.0 / 11.5	-1.8 / 12.0	-1.2	-1.4 / 12.0	-1.2 / 11.8
+15	12.174		-0.0 / 12.0	-1.0	-0.0 / 12.0	

Width of Road 24'
Grade 7%
Slope 1½ to 1

1636

1637

East Approach of Trestle at County Road Bridge
Sta D 743+0.5

	Lt.			C		Rt.		
1+77.26	-12.1 29.2	-11.9 16.3	-10.1 11.0	-5.0 2.0	-4.7	-4.7 11.0	-4.9 12.0	-13.6 28.6	-12.5 30.7
2+0.0	-10.6 26.9	-10.5 20.0	-7.0 11.0	-3.5 5.0	-3.4	-3.3 7.0	-4.1 11.0	-11.8 26.7	-12.2 29.3
2+25	-9.2 24.8	-8.5 20.8	-4.1 11.0	-2.0 9.0	-2.0	-2.0 7.8	-3.1 11.0	-9.5 23.6	-9.1 24.7
2+50	-7.5 22.3	-1.9 11.0	-0.1 8.0	0.0	0.0 6.0	-2.3 11.0	-8.8 23.6		
2+75	-3.9 16.9	-1.4 11.0	-0.3 9.0	0.0	+0.3 11.0				
2+96.07 ΔEc	-2.5 19.8	-1.9 11.0	-0.1 7.0	0.0	-0.8 9.0	-1.1 11.0	-3.6 16.4		

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Final Estimate No 145

1638

Grade Road Crossing. "D" 777+46.0

Sta. "D" 777+46 △ 0+00.0 △ 90°0.0 Rt	Grade	Lt	C	Rt		
0+65			0.0 9.0	0.0	0.0 9.0	
0+90	2.56%	-1.7 11.5	-1.7 9.0	-1.7	-1.7 9.0	-1.7 11.5
0+154	2.07%	-16.0 23.0	-16.4 9.0	-16.4	-16.7 9.0	-16.5 33.8
1+00	1.57%	-10.6 24.9	-10.8 9.0	-11.0	-10.8 9.0	-10.9 25.4
1+50	1.57%	-5.8 17.7	-5.8 9.0	-5.8	-5.8 9.0	-5.8 17.7
2+07.0	5.9		0.0 9.0	0.0	0.0 9.0	

Page 66 To Used In
Final Estimate No 15-0

1639

Pages 67 T[illegible] 68 T[illegible] in
Final Est[illegible] 10/31

1640

Sta. Cross Sections of Lands Johnston Estate, for Borrow Pit

Lt. C. Rt.

9 +65	0.0 5.0	+2.3 10	+2.4	+3.2 10	+2.7 20	+3.8 30	+4.1 40	+2.0 50	0.0 60
+50		0.0 4.0	+1.0	+3.2 5.0	+3.8 10.0	+4.7 30	+4.2 32	+3.8 40	+4.1 50	0.0 64
9 +0.0	0.0 17	+3.2 10	+3.6	+4.1 10	+4.6 20	+3.1 30	0.0 38		
+50	0.0 1.8	+1.5 10	+2.9	+2.9 8.0	+0.8 10	0.0 18			
8 +0.0	0.0 35	+1.1 30	+3.1 20	+2.9 10	+2.8 5	+0.8	0.0 4		

1491

1642

70

Original Cross Sections of Borrow Pit

Aug. 12-05 12'

H 748	7.7 / 73.0	7.9 / 100.0	7.8 / 125.0	7.8 / 185.0			
+50	7.0 / 65.0	8.4 / 100.0	7.9 / 135.0	7.7 / 156.0	7.7 / 170.0	7.6 / 185.0	
747	7.1 / 67.0	9.1 / 100.0	7.0 / 130	7.0 / 156.0	7.0 / 171.0	7.0 / 185.0	7
+78 Δ EC	6.9 / 63.0	6.4 / 100.0	7.1 / 135.0	6.9 / 155.0	6.6 / 174.0	7.0 / 185.0	
+50	5.8 / 66.0	5.6 / 100.0	6.0 / 135.0	6.1 / 156.0	5.6 / 167.0	6.1 / 185.0	
746	5.1 / 68.0	5.3 / 100.0	5.7 / 135.0	6.2 / 147.0	6.2 / 160.0	7.0 / 185.0	
+50	5.0 / 68.0	5.0 / 100.0	5.4 / 135.0	5.7 / 147.0	6.9 / 170.0	7.0 / 185.0	
745	5.0 / 68.0	5.3 / 100.0	5.7 / 135.0	5.9 / 148.0	7.0 / 157.0	6.8 / 170.0	7.1 / 185.0
+50	5.2 / 67.0	5.7 / 100.0	7.2 / 127.0	7.3 / 125.0	7.6 / 147.0	7.0 / 153.0	7.7 / 170.0	7.7 / 185.0
744	4.0 / 70.0	4.5 / 100.0	5.6 / 116.0	7.2 / 135.0	7.7 / 151.0	8.1 / 185.0	
+50	5.3 / 69.0	4.1 / 100.0	4.9 / 135.0	5.7 / 176.0	7.5 / 169.0	8.0 / 185.0	
743	4.1 / 62.0	4.0 / 100.0	4.6 / 135.0	4.9 / 157.0	5.8 / 174.0	7.5 / 185.0	
+50	6.5 / 64.0	4.4 / 100.0	3.6 / 135.0	4.4 / 143.0	5.7 / 148.0	5.9 / 167.0	7.2 / 185.0
742	10.2 / 35.0	5.9 / 64.0	4.5 / 100.0	5.0 / 136.0	7.2 / 148.0	7.2 / 174.0	7.7 / 180.0	7.2 / 185.0
741 +50							

1643

tangent produced ahead

1644

Table IV.—Minutes in Decimals of a Degree.

1′	.0167	11′	.1833	21′	.3500	31′	.5167	41′	.6833	51′	.8500
2	.0333	12	.2000	22	.3667	32	.5333	42	.7000	52	.8667
3	.0500	13	.2167	23	.3833	33	.5500	43	.7167	53	.8833
4	.0667	14	.2333	24	.4000	34	.5667	44	.7333	54	.9000
5	.0833	15	.2500	25	.4167	35	.5833	45	.7500	55	.9167
6	.1000	16	.2667	26	.4333	36	.6000	46	.7667	56	.9333
7	.1167	17	.2833	27	.4500	37	.6167	47	.7833	57	.9500
8	.1333	18	.3000	28	.4667	38	.6333	48	.8000	58	.9667
9	.1500	19	.3167	29	.4833	39	.6500	49	.8167	59	.9833
10	.1667	20	.3333	30	.5000	40	.6667	50	.8333	60	1.0000

Table V.—Inches in Decimals of a Foot.

1-16 .0052	3-32 .0078	1/8 .0104	3-16 .0156	1/4 .0208	5-16 .0260	3/8 .0313	1/2 .0417	5/8 .0521	3/4 .0625	7/8 .0729

1 .0833	2 .1667	3 .2500	4 .3333	5 .4167	6 .5000	7 .5833	8 .6667	9 .7500	10 .8333	11 .9167

Table VI.—Radii, Ordinates and Deflections.

Deg.	Radius	Mid Ord	Tan Def.	Chd. Def.	Def for 1 Foot	Deg.	Radius	Mid Ord	Tan Def	Chd Def.	Def for 1 Foot
0° 10′	34377.	.036	.145	.291	0.05′	7°	819.0	1.528	6.105	12.21	2.10′
20	17189.	.073	.291	.582	0.10	20′	781.8	1.600	6.395	12.79	2 20
30	11459.	.109	.436	.873	0.15	30	764.5	1.637	6.540	13.08	2.25
40	8594.4	.145	.582	1.164	0.20	40	747.9	1.673	6.685	13.37	2.30
50	6875.5	.182	.727	1.454	0.25	8	716.8	1 746	6.976	13.95	2.40
1	5729.6	.218	.873	1.745	0.30	20	688.2	1.819	7.266	14.53	2.50
10	4911.2	.255	1.018	2.036	0.35	30	674 7	1 855	7.411	14.82	2.55
20	4297 3	.291	1.164	2.327	0.40	40	661.7	1.892	7.556	15.11	2.60
30	3819.8	.327	1.309	2.618	0.45	9	637.3	1.965	7.846	15.69	2.70
40	3437.9	.364	1.454	2.909	0.50	20	614.6	2 037	8.136	16 27	2.80
50	3125 4	.400	1.600	3.200	0.55	30	603.8	2.074	8.281	16.56	2.85
2	2864 9	.436	1.745	3 490	0.60	40	593 4	2.110	8.426	16 85	2.90
10	2644.6	.473	1.891	3.781	0.65	10	573.7	2 183	8.716	17 43	3.00
20	2455.7	.509	2.036	4.072	0.70	30	546.4	2 292	9.150	18 30	3.15
30	2292 0	.545	2.181	4.363	0.75	11	521.7	2.402	9.585	19.16	3.30
40	2148.8	.582	2.327	4.654	0.80	30	499.1	2 511	10.02	20.04	3.45
50	2022.4	.618	2 472	4.945	0.85	12	478.3	2.620	10.45	20.91	3.60
3	1910.1	.655	2.618	5.235	0 90	30	459 3	2.730	10.89	21 77	3.75
10	1809.6	.691	2.763	5.526	0.95	13	441.7	2 839	11.32	22 64	3.90
20	1719.1	727	2.908	5.817	1.00	30	425.4	2.949	11.75	23.51	4.05
30	1637 3	.764	3.054	6.108	1.05	14	410 3	3.058	12.18	24 37	4 20
40	1562.9	.800	3.199	6.398	1.10	30	396 2	3.168	12 62	25.24	4.35
50	1495.0	.836	3.345	6.689	1.15	15	383.1	3.277	13 05	26.11	4 50
4	1432.7	.873	3.490	6.980	1.20	30	370 8	3.387	13.49	26.97	4.65
10	1375.4	.909	3 635	7.271	1.25	16	359 3	3.496	13.92	27 84	4 80
20	1322.5	.945	3.718	7.561	1.30	30	348.5	3.606	14 35	28 70	4 95
30	1273.6	.982	3.926	7.852	1.35	17	338 3	3 716	14 78	29.56	5 10
40	1228.1	1.018	4.071	8.143	1.40	18	319 6	3.935	15 64	31.29	5.40
50	1185.8	1.055	4.217	8.433	1.45	19	302 9	4.155	16 51	33.01	5 70
5	1146.3	1 091	4 362	8.724	1 50	20	287 9	4.374	17.37	34.73	6 00
10	1109.3	1.127	4.507	9.014	1.55	21	274.4	4.594	18.22	36 44	6 30
20	1074.7	1.164	4.653	9.305	1.60	22	262 0	4.814	19 08	38.16	6.60
30	1042.1	1 200	4.798	9.596	1.65	23	250 8	5 035	19.94	39 87	6 90
40	1011.5	1.237	4.943	9.886	1 70	24	240 5	5.255	20 79	41.58	7.20
50	982.6	1.273	5 088	10.18	1.75	25	231 0	5.476	21 64	43.28	7.50
6	955.4	1 309	5.234	10.47	1.80	26	222.3	5.697	22 50	44.99	7.80
10	929.6	1.346	5.379	10.76	1.85	27	214.2	5,918	23.35	46 69	8 10
20	905.1	1 382	5.524	11 05	1 90	28	206 7	6.139	24.19	48.38	8 40
30	881.9	1.418	5.669	11.34	1 95	29	199 7	6.360	25.04	50.07	8.70
40	859.9	1.455	5.814	11.63	2.00	30	193 2	6.583	25.88	51.76	9.00

1645